

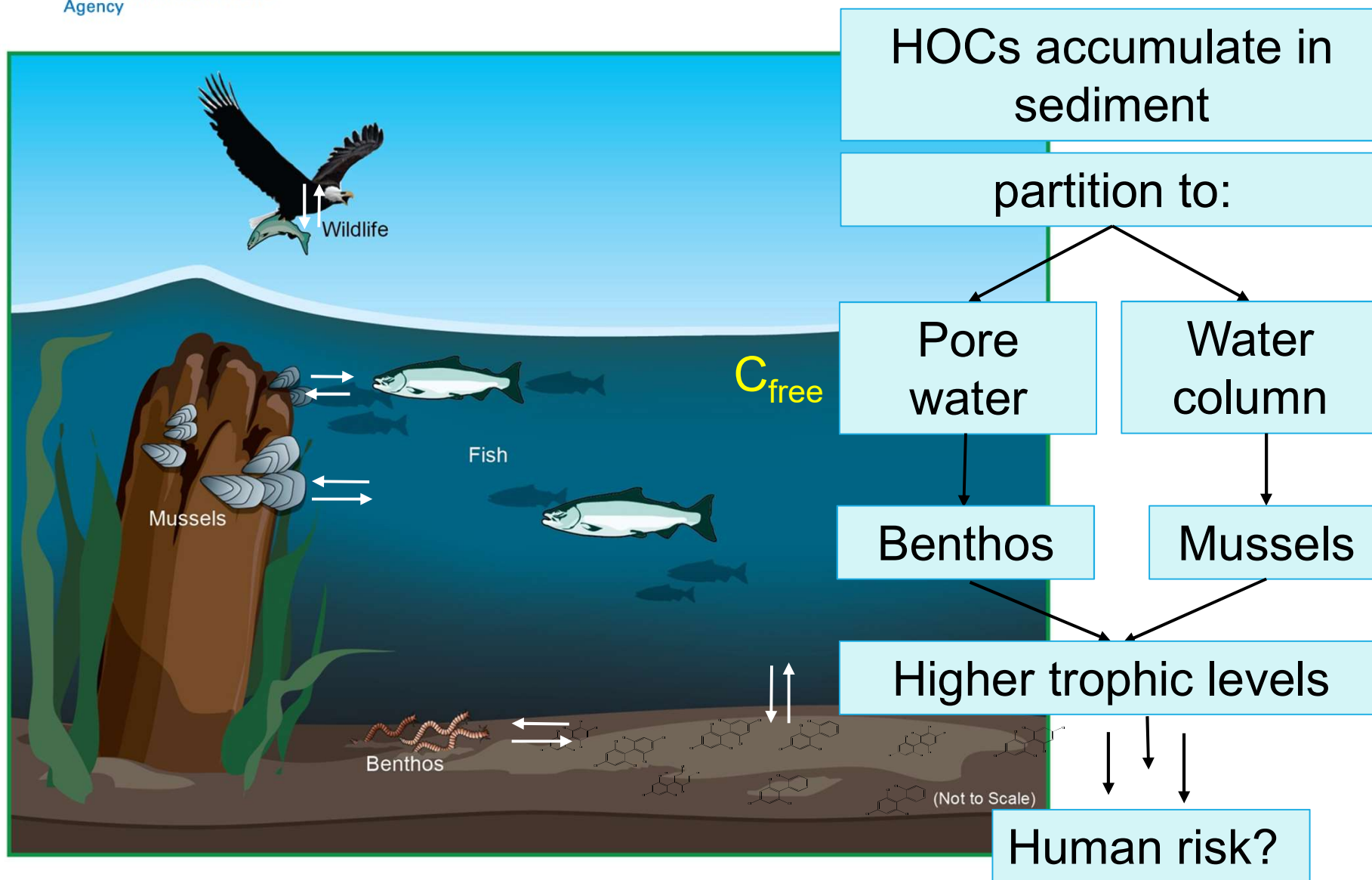
# Measuring Freely Dissolved Water Concentrations of PCBs Using Passive Samplers and Performance Reference Compounds (PRCs)

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# Introduction



What is  $C_{\text{free}}$ ?

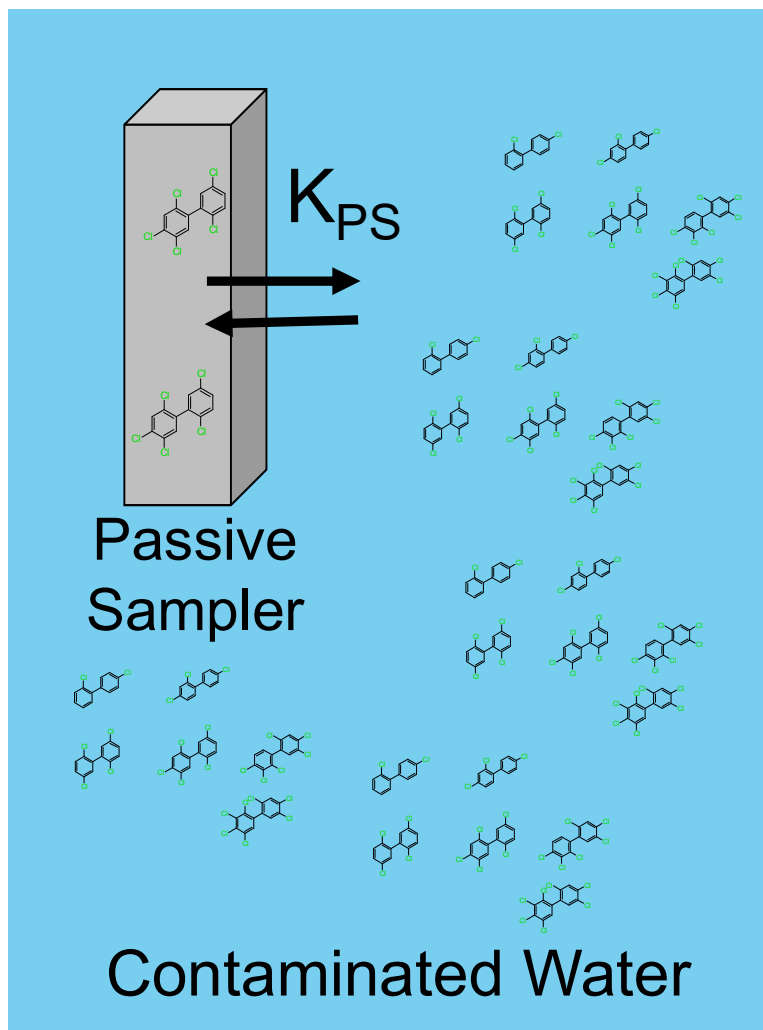
- dissolved and bioavailable HOC concentration in water
- often pg/L – ug/L range
- used as an exposure measure in risk management

How do you measure  $C_{\text{free}}$ ?

## Passive Sampling

- PCBs
- PAHs
- DDTs
- Dioxins
- PBDEs
- accumulate HOCs proportionately to bioaccumulation

# Passive Sampling

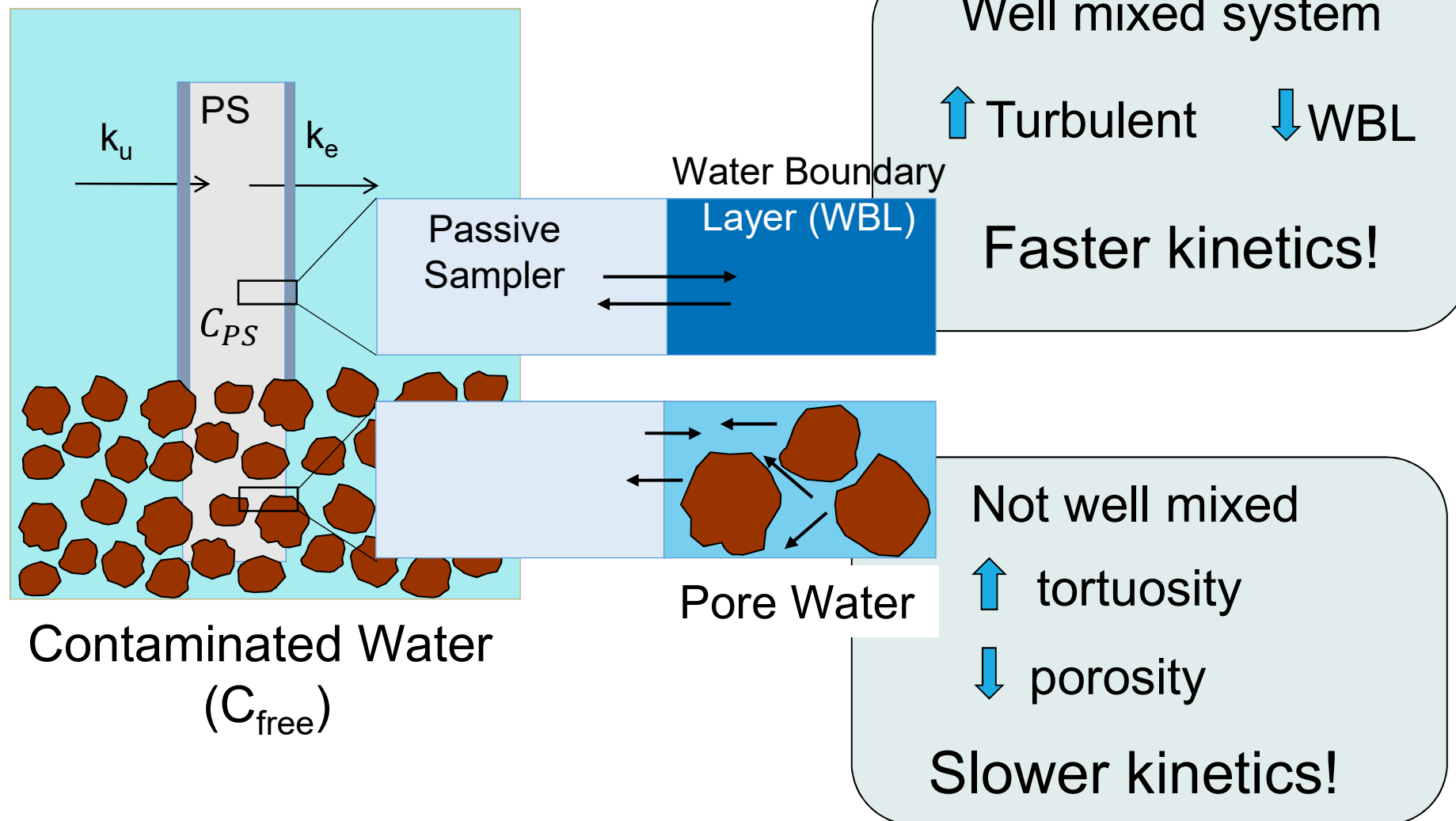


- Hydrophobic organic compounds (HOCs) concentrate in hydrophobic sampler
- Compounds will equilibrate ( $K_{PS}$ ):

$$K_{PS} = \frac{C_{PS}^{\infty}}{C_{free}}$$

- Must know  $K_{PS}$
- Must be at equilibrium (takes weeks-months)

# In Situ Passive Sampling

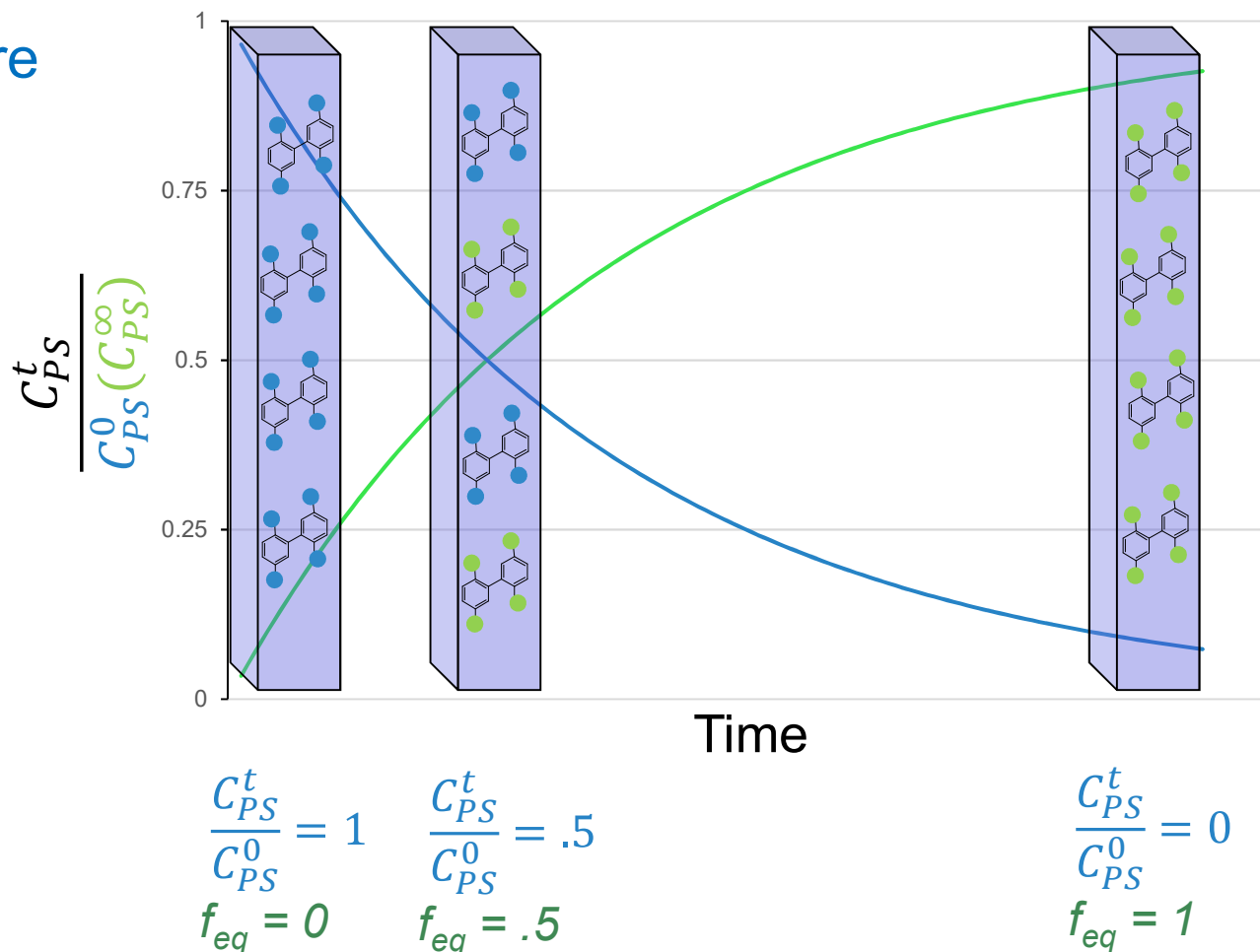


# Performance Reference Compounds (PRCs)

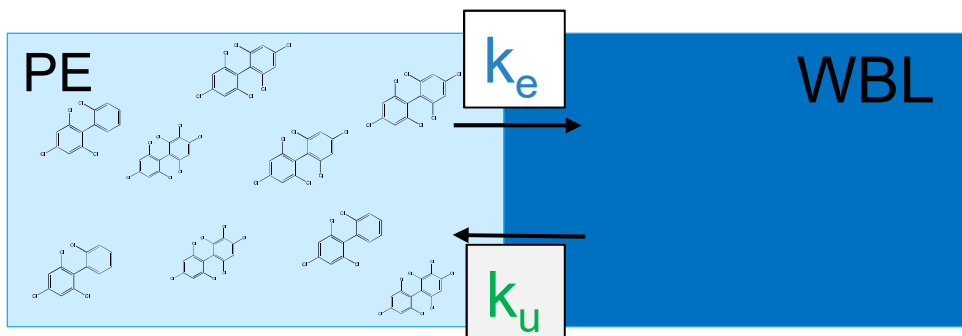
PRC:

- Loaded into PS before deployment
- Similar to the target HOCs
- Non-interfering
- Ensure equilibrium
- Correct for non-equilibrium using fractional equilibrium ( $f_{eq}$ )

$$f_{eq} = 1 - \frac{C_{PS}^t}{C_{PS}^0}$$



# 1<sup>st</sup> Order Model



The model:

$$\frac{dC_{PS}}{dt} = k_u C_{free} - k_e C_{PS}$$

The Solution:

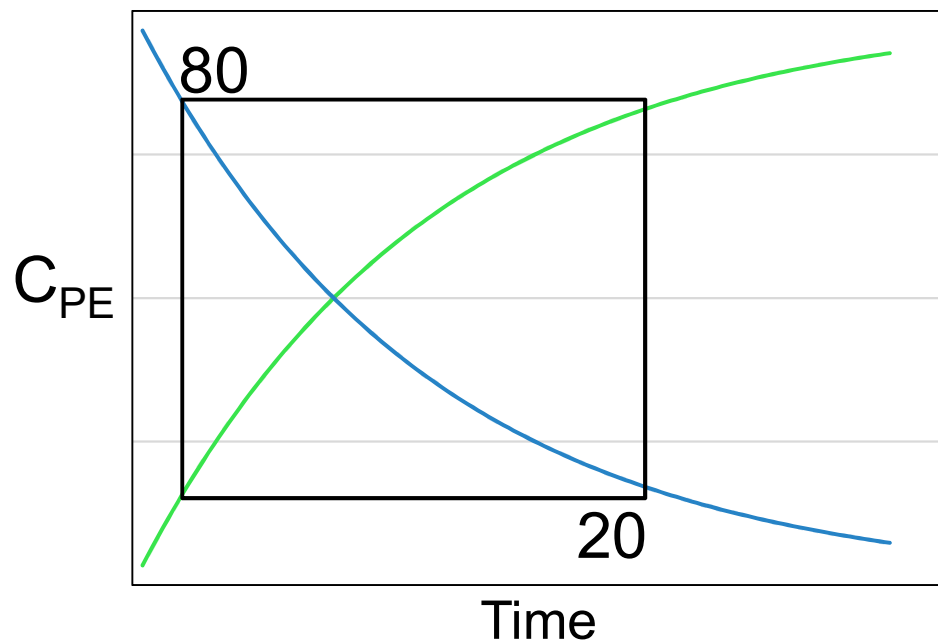
$$C_{PS} = \frac{k_u}{k_e} C_{free} (1 - e^{-k_e t})$$

$$k_e = - \frac{\ln \left( \frac{C_{PRC}^t}{C_{PRC}^0} \right)}{t}$$

The drawback:

Need a PRC for each HOC

Limited sample range “80:20”



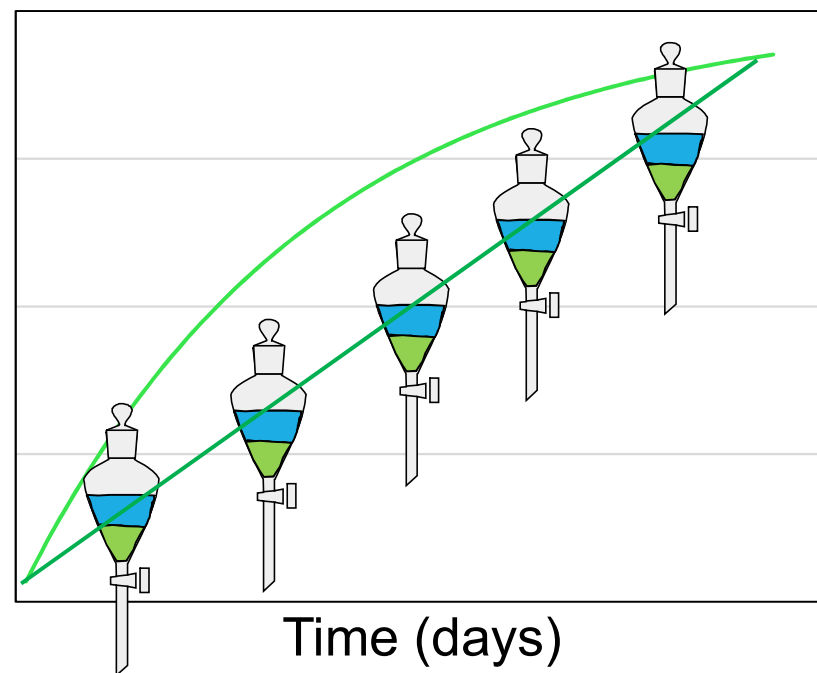
# Sampling Rate ( $R_s$ ) Model

- $R_s$  - the volume of contaminated water “extracted” over time (L/day)

Model:

$$R_s = k_e K_{PW} m_{PS}$$

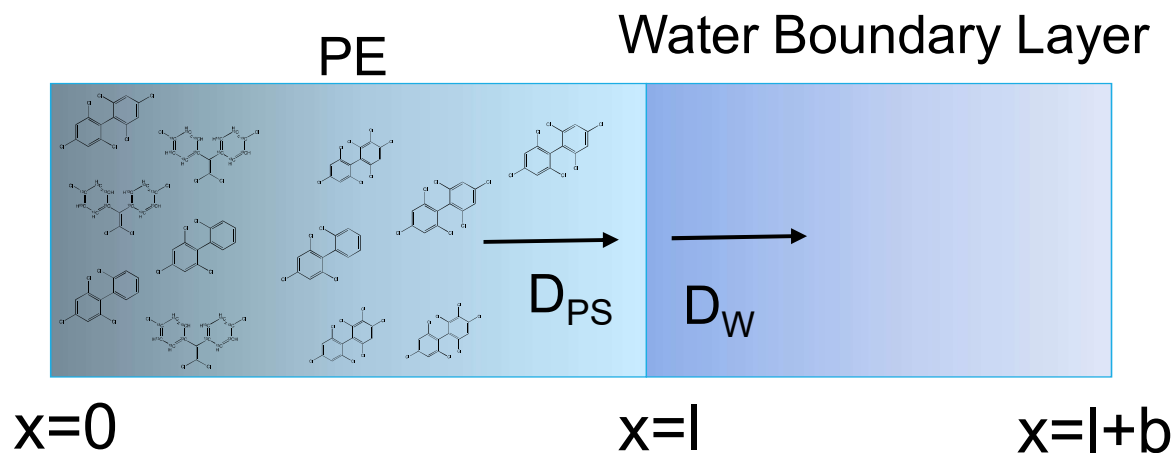
$$f = e^{\left(\frac{-R_s t}{K_{PW} m_{PS}}\right)}$$



- Interpolating  $R_s$  not always easy
- Challenging depending on phase uptake control.



# Diffusion Model



The model:

$$D_{PS} \frac{\delta C_{PS}}{\delta t} = D_W \frac{\delta^2 C_W}{\delta x^2}$$

$$\frac{\delta C_{PS}}{\delta t} = D_{PS} \frac{\delta^2 C_{PS}}{\delta x^2}$$

The Solution:

$$\frac{\hat{C}_{PRC}^t}{C_{PRC}^0} = \frac{1}{s} - \left\{ s^{3/2} \left( \frac{K_{PS} \tanh \frac{\hat{\partial} \sqrt{s}}{\sqrt{\psi}}}{\sqrt{\psi}} + \coth \sqrt{s} \right) \right\}^{-1}$$

The drawback:

Requires  $D_{PS}$  and  $D_W$ , and solution is in LaPlace space

# There's a GUI for that!

Graphical User Interfaces (GUI) exist to help calculate  $f_{eq}$  for these models

- $R_s$  model (excel spreadsheet)

[www.rs.passivesampling.net/](http://www.rs.passivesampling.net/)

- LDPE in sediments

[www.serdp-estcp.org](http://www.serdp-estcp.org) ER-200915

- LDPE in water column

- Coming Soon!

- SPME

[www.depts.ttu.edu/ceweb/groups/reiblesgroup/downloads.html](http://www.depts.ttu.edu/ceweb/groups/reiblesgroup/downloads.html)

To Use:

- $f_{eq}$  or  $\frac{C_{PRC}^t}{C_{PRC}^0}$
- PS details
- Deployment time
- Porosity
- GUI will give  $f_{eq}$  for target HOCs!





$$C_{free} = \frac{C_{PS}^t}{K_{PS} * f_{eq}}$$

# Study Objectives

- Measure  $C_{\text{free}}$  suite of PCBs in New Bedford Harbor water column
- Determine precision of the PCB measurements using passive sampling
- Determine the best model for estimating equilibrated passive sampler concentrations

# Study Design

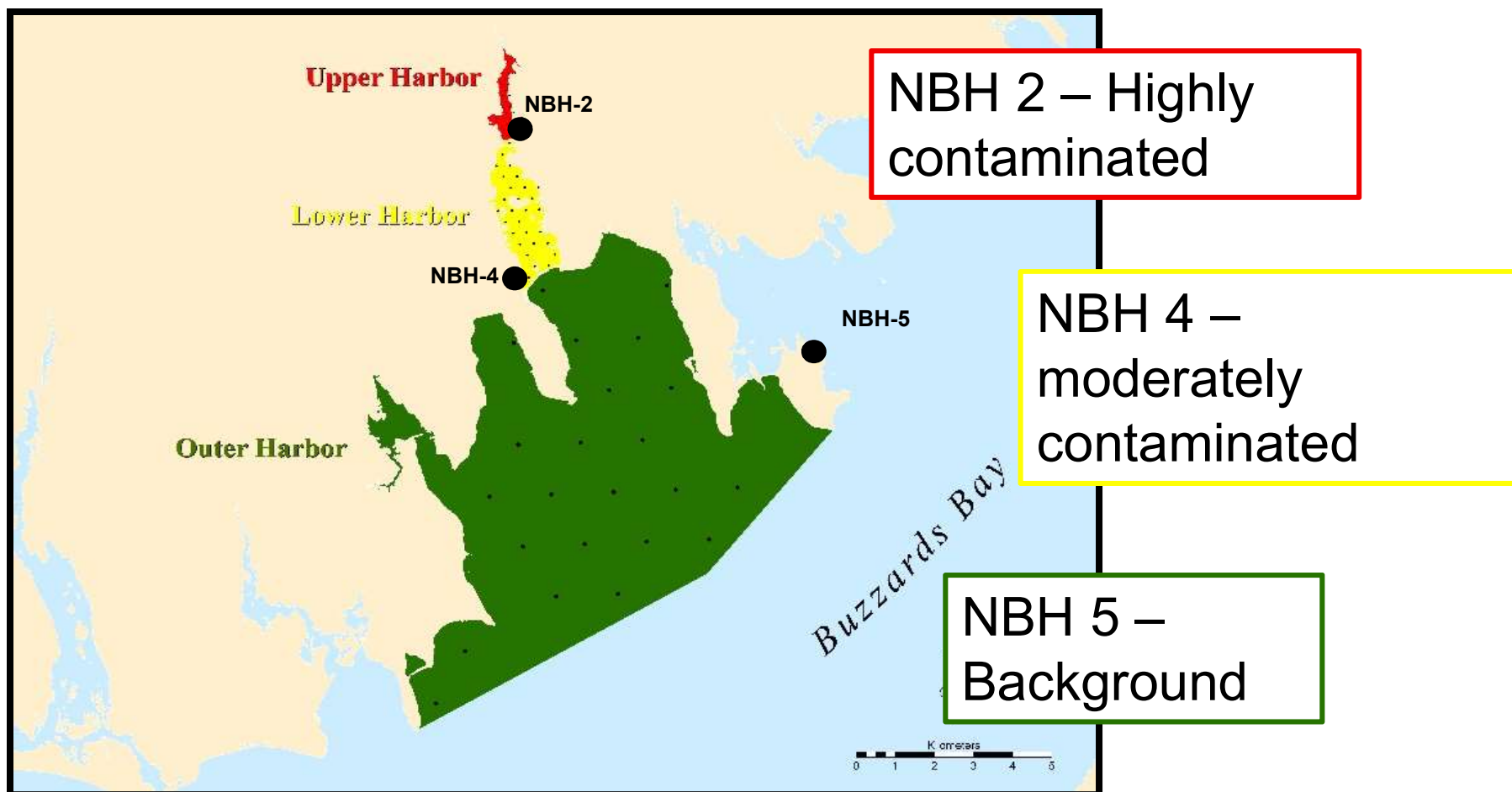
## LDPE thicknesses

	12.7 $\mu\text{m}$
	25.4 $\mu\text{m}$
	50.8 $\mu\text{m}$
	76.2 $\mu\text{m}$

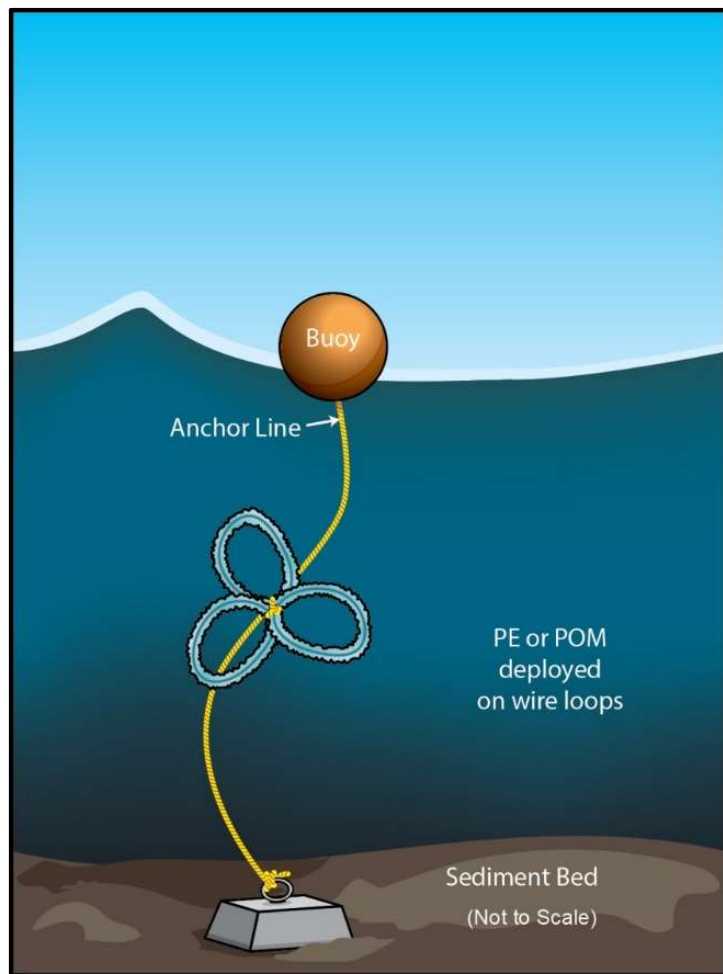
- LDPE were pre-loaded with six  $^{13}\text{C}_{12}$ -PCBs as PRCs Booij et al. (2002)
- One congener for each homolog  $\text{Cl}_2 - \text{Cl}_7$

- Four different thicknesses = different  $f_{eq}$  per sampler and congener
- Different thicknesses allowed comparisons within a model

# New Bedford Harbor, MA, USA



# Deployment

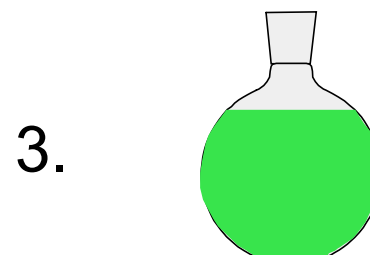
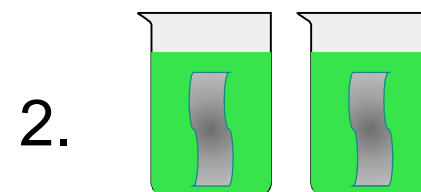
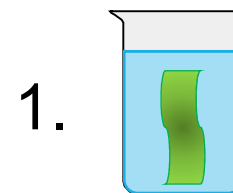


- LDPE deployed in triplicate
- 1 m above sediment surface
- 28 d deployment

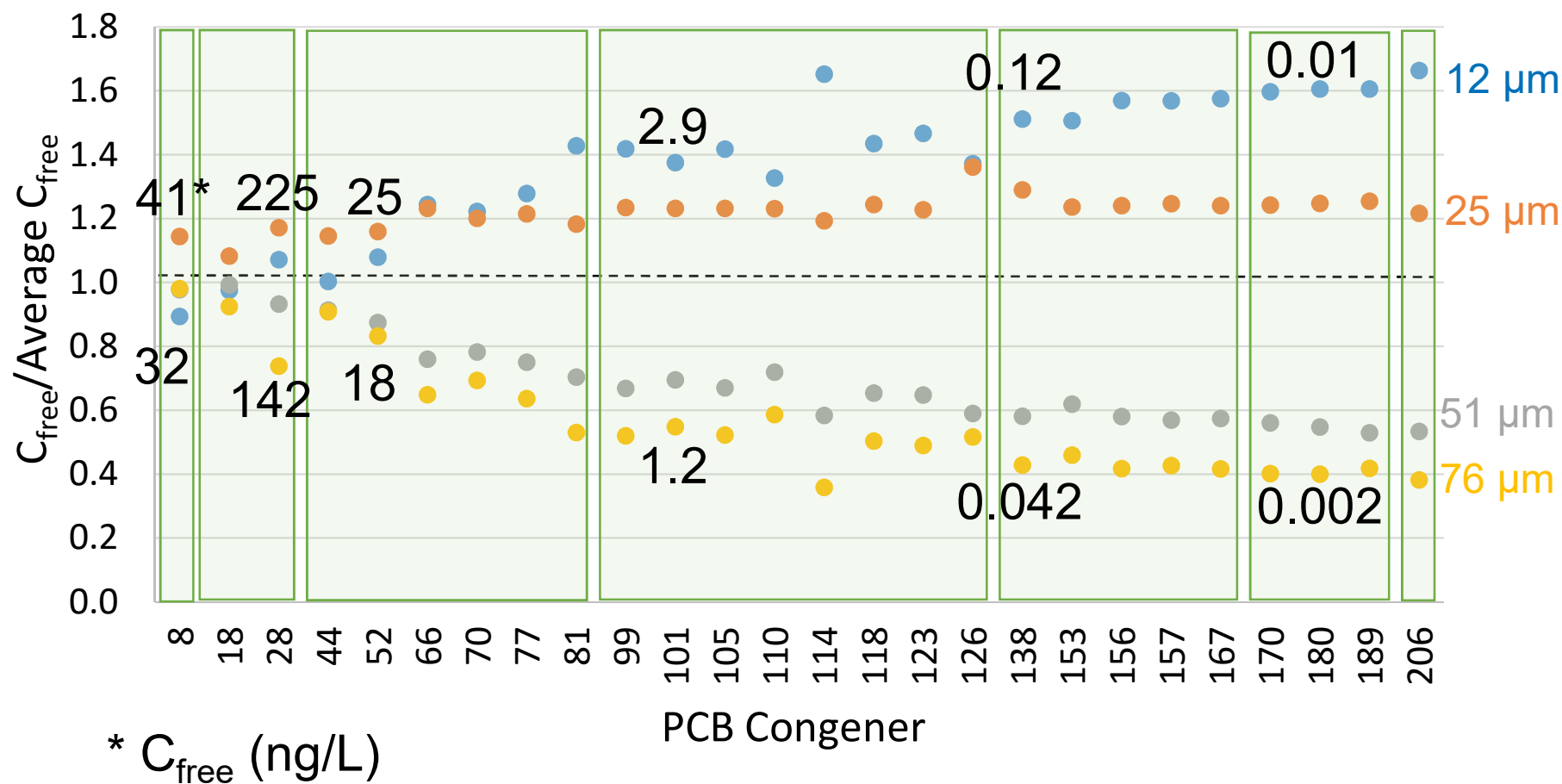
# Extraction

1	Extract passive sampler
2	Repeat extraction 2-3x
3	Combine extracts
4	Concentrate extract
5	Transfer to storage vial
6	Analyze GC-MS

Surrogate Standard	Average Recovery
$^{13}\text{C}$ -PCB 9	$51 \pm 9$
$^{13}\text{C}$ -PCB 118	$83 \pm 7$
$^{13}\text{C}$ -PCB 188	$76 \pm 6$

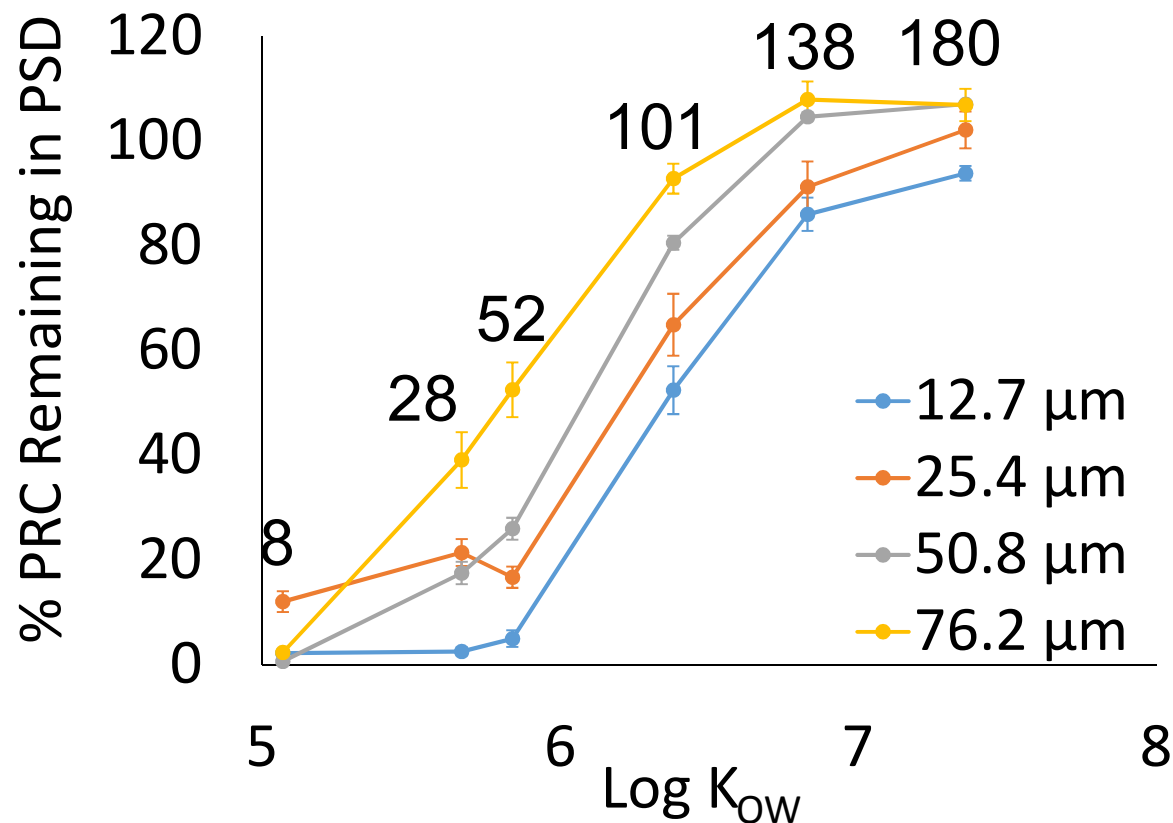


# Are you at Equilibrium?



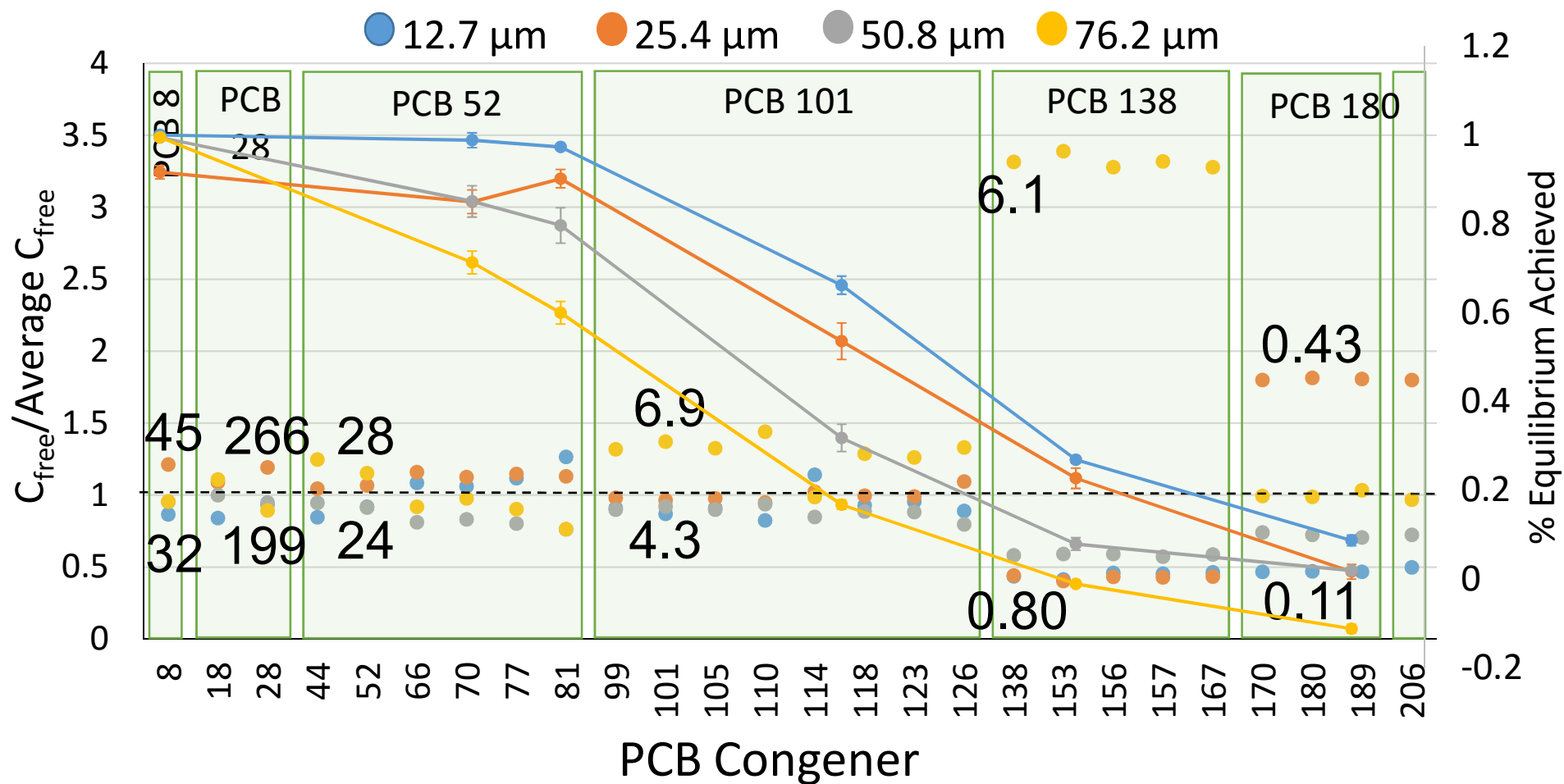


# PRC Results



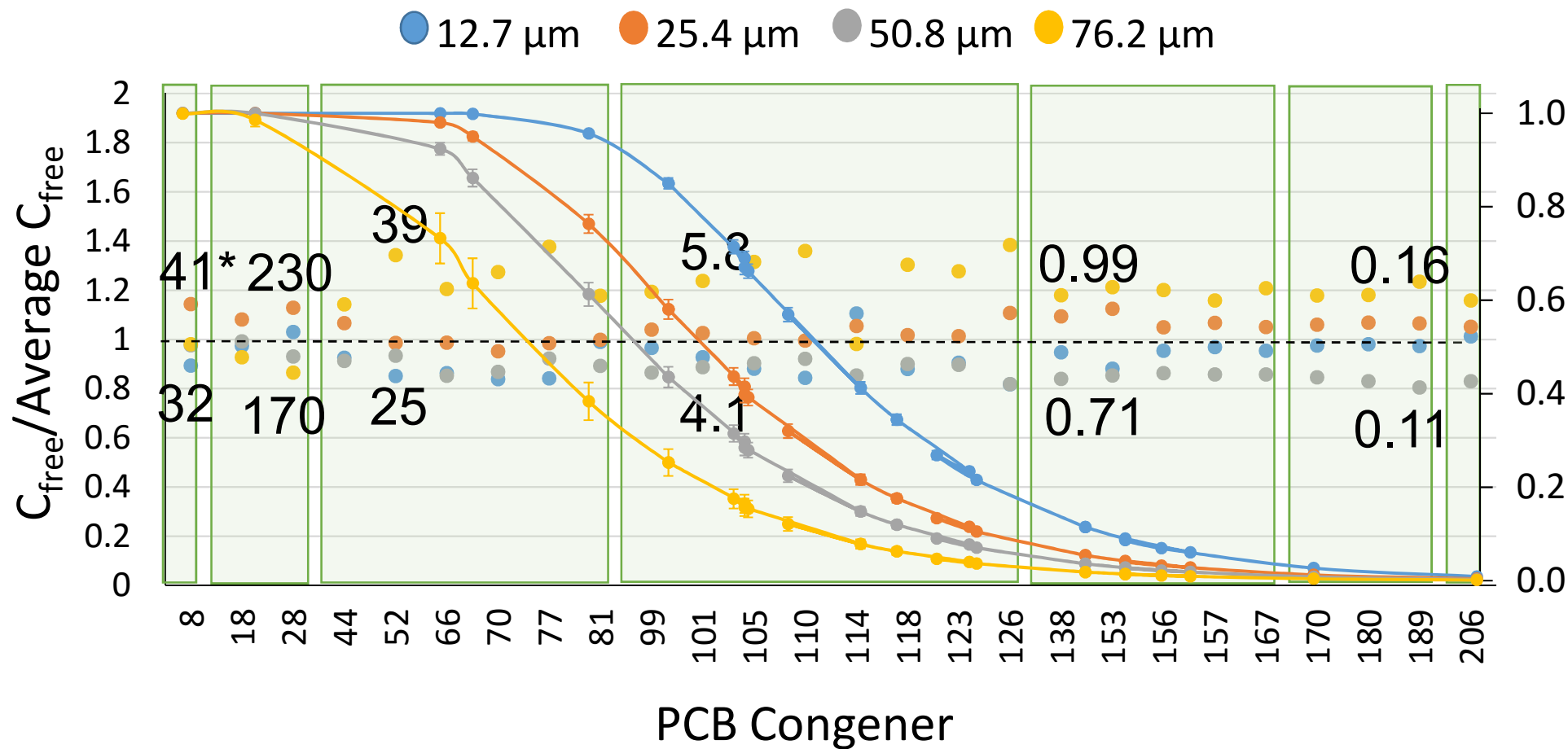
- Smaller PRCs – faster kinetics
- Thicker passive sampler – retained more PRC

# 1<sup>st</sup> Order Model



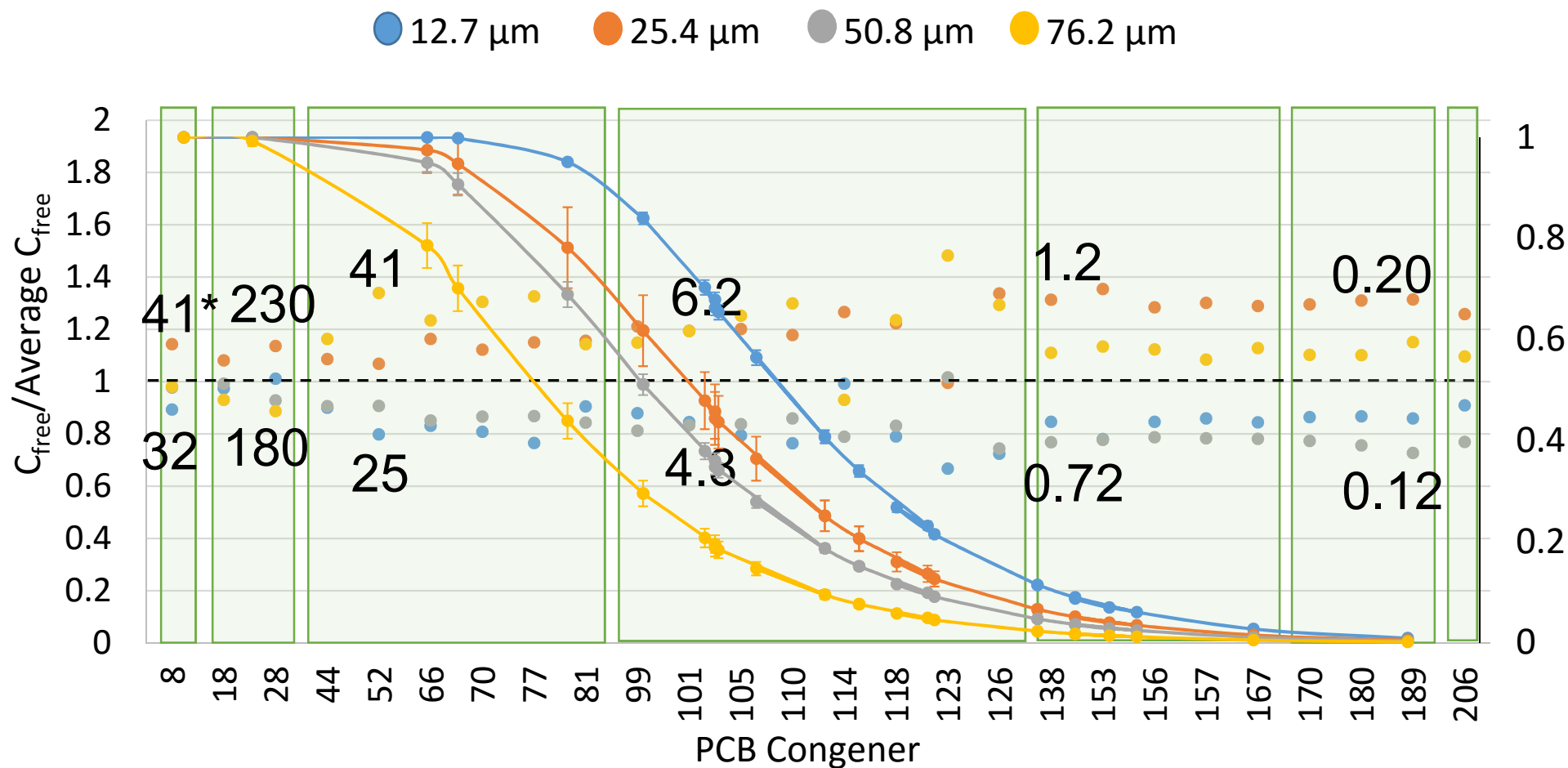
\*  $C_{\text{free}}$  (ng/L)

# Rs Model



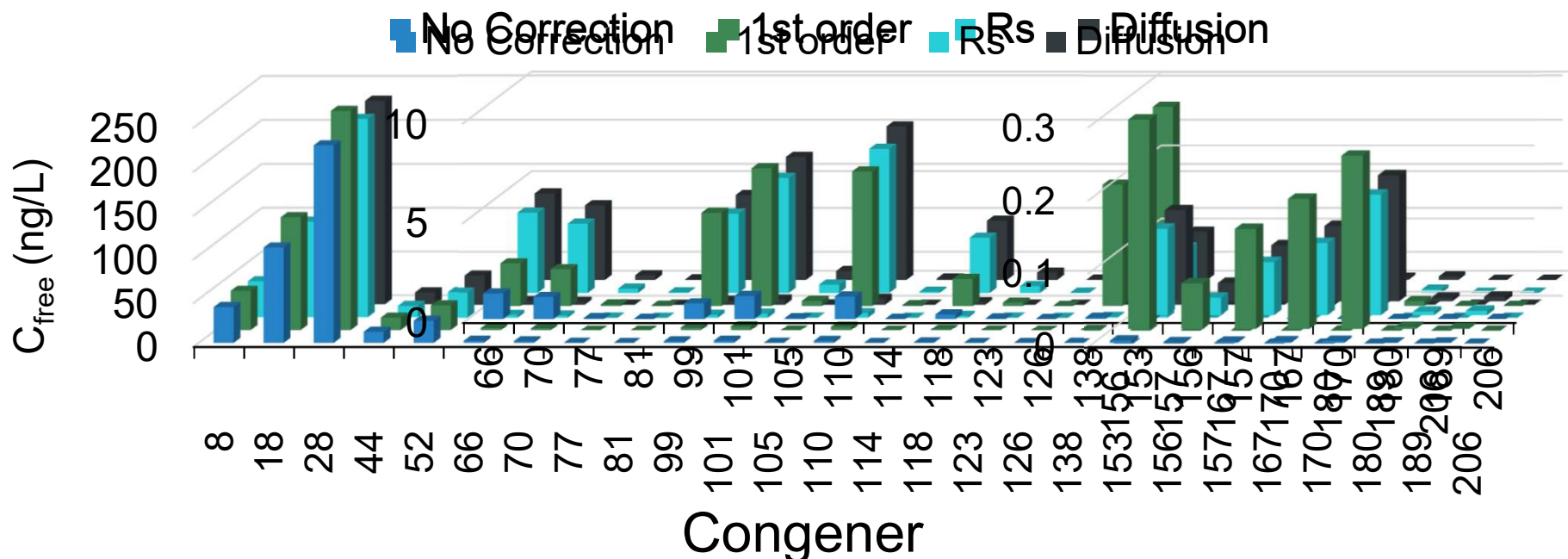
\*  $C_{\text{free}}$  (ng/L)

# Diffusion Model



\*  $C_{\text{free}}$  (ng/L)

# Water Concentrations



Using 76 $\mu$ m LDPE data:

- Most water soluble PCBs – highest  $C_{\text{free}}$
- As compounds get bigger model correction increases
- $C_{\text{free}}$  was measured from  $1.07 \times 10^{-5}$  – 200 ng/L

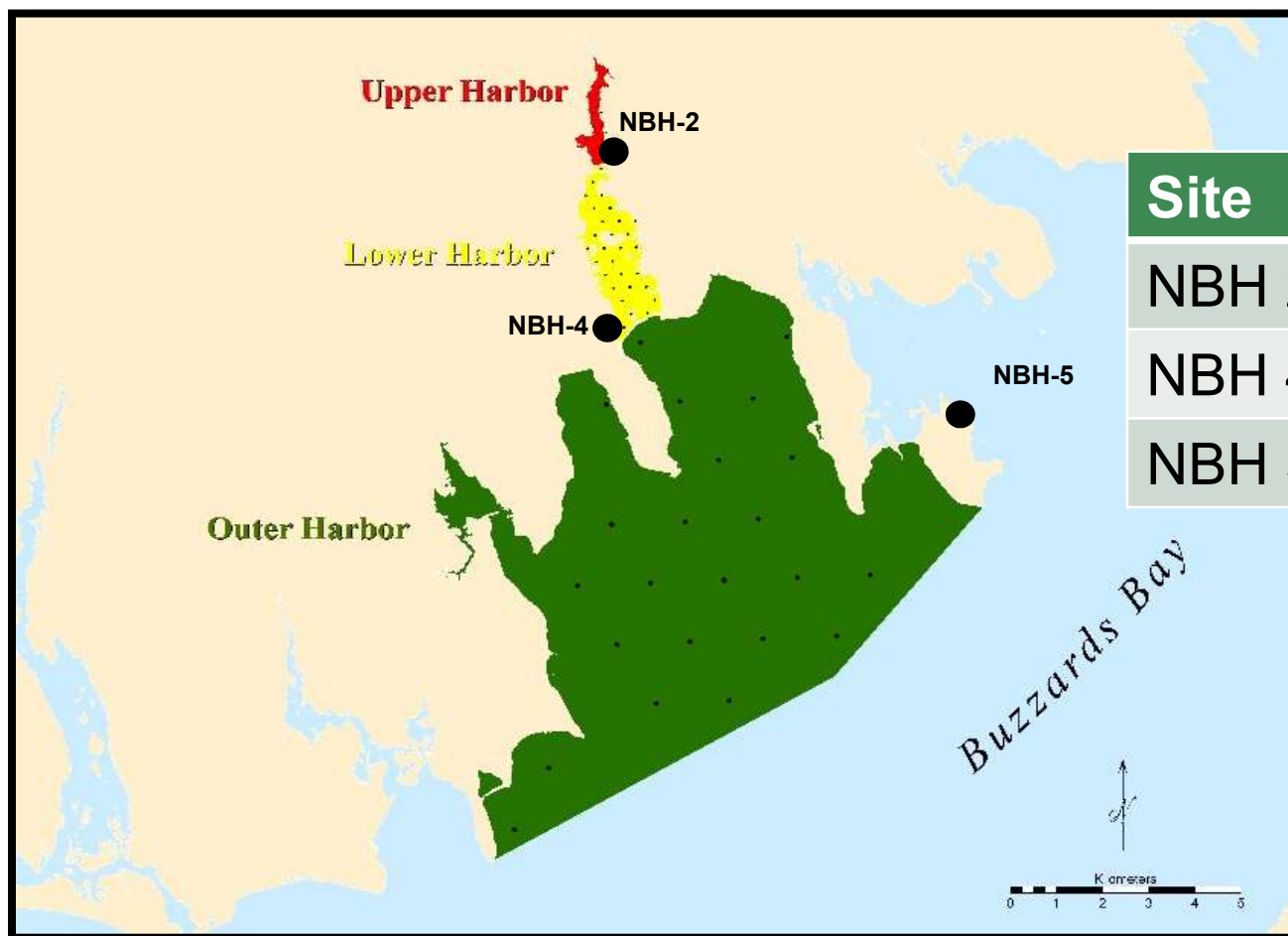
# Total PCB trends

$C_{\text{free}}$   $\Sigma$ PCB (ng/L) by model and sampler

LDPE Thickness	No Correction	1st order	Rs	Diffusion	Average
12.7	385	396	395	396	$396 \pm 0.04\%$
25	427	505	444	463	$470 \pm 5\%$
50	351	423	382	388	$398 \pm 5\%$
76	305	456	387	401	$415 \pm 7\%$
Average	$367 \pm 12\%$	$445 \pm 9\%$	$402 \pm 6\%$	$412 \pm 7\%$	

- RSD increased with thickness
- 1<sup>st</sup> order model had the highest RSD

# Final $C_{\text{free}}$



Site	$\Sigma\text{PCB}^*$
NBH 2	400 - 500 (ng/L)
NBH 4	36 – 48
NBH 5	0.14 – 0.28

\*Non corrected data  
not included

# Conclusions

- Using LDPE, the measurement of PCB  $C_{\text{free}}$  is viable and precise
- Total PCB agreed better between models using the same dataset than between a single model with different datasets
  - Model may be chosen by laboratory –  $R_S$  or Diffusion recommended
- Results where  $f_{eq}$  is near zero should be used with discretion



# Acknowledgments

Thank you:

Barbara Bergen

Don Cobb

Michaela Cashman

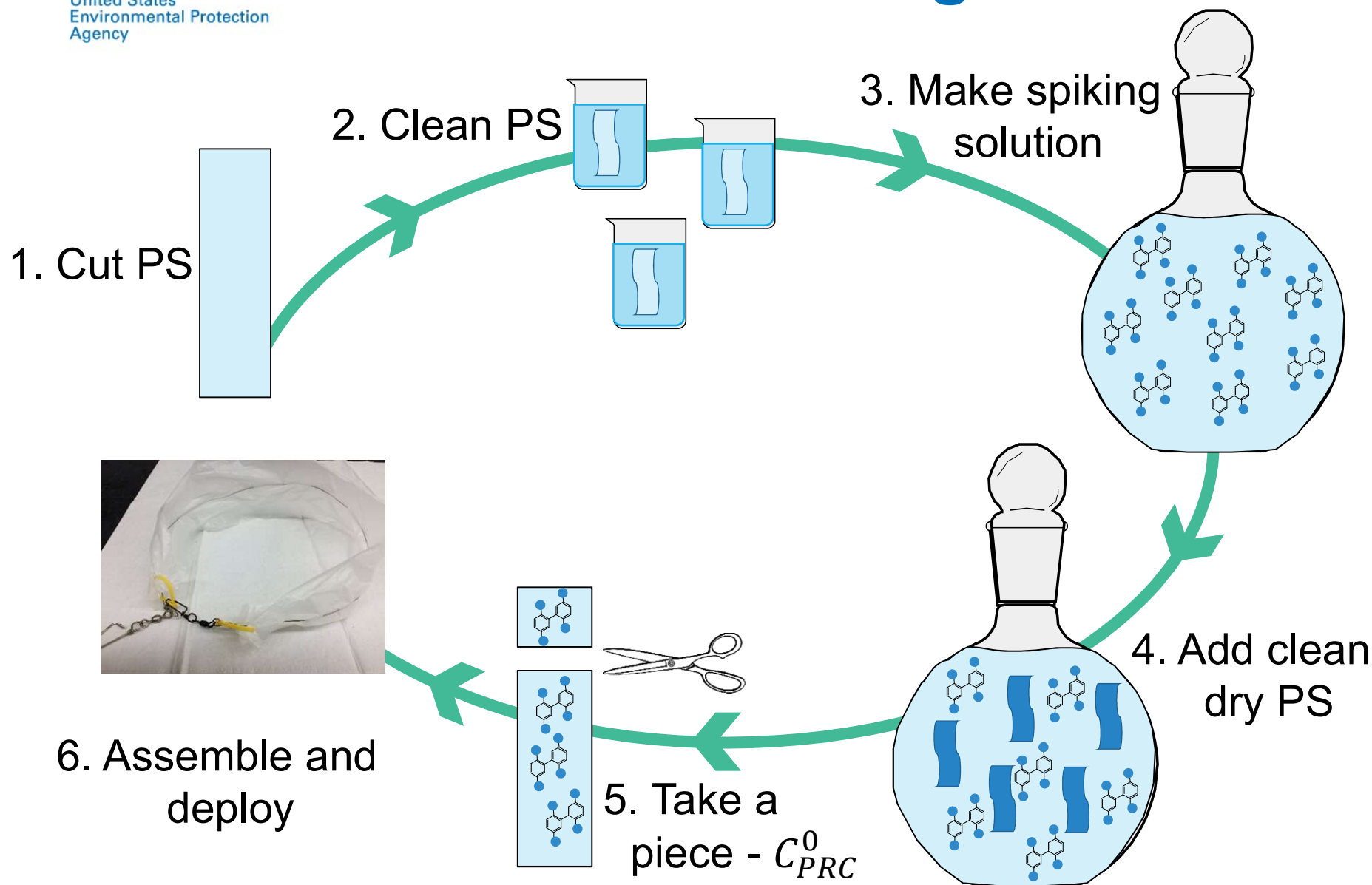
Mark Cantwell

Dave Katz



# Questions?

# PRC Loading



# Passive Samplers



## Solid Phase Microextraction (SPME)

- Polydimethylsiloxane (PDMS)
- solventless workup
- fragile

## Semi-Permeable Membrane Device (SPMD)

- lipid filled tubing
- susceptible to breakage
- complicated extraction and analysis



## Thin Sheets

- Low Density Polyethylene (LDPE)
- Polyoxymethylene (POM)
- Silicone

- less sensitive to breakage
- simple geometry
- economical and commercially available

